

台電 BWRs/PWRs 水化學控制最適化進展



台電核發處 核能化學組
朱方

中華民國98年12月16日

大綱 I

- BWR/PWR 水化學控制為什麼需要**最適化**(Optimization) ? ►
- BWR/PWR 水化學控制最適化(OWC)**關鍵參數** ►
- 從ECP及pH酸鹼值控制看臺電 BWR/PWR水化學最適化控制策略的形成與進展
- [OWC in Taipower BWRs](#)

核一、二廠目前IGSCC Mitigation Program

- ◆ HWC-L : 0.5 ppm (2006第四季) → HWC-M : **1.2/1.1/1.0** ppm (2009下半年)
- ◆ IGSCC mitigation effectiveness evaluation ►
- ◆ After HWC :
 - 乾井管路Dose Rate變化 → Shutdown dose rate mitigation strategies after HWC-M.
 - FW Fe變化, RW Cu變化 ►
 - Application of BWRVIP-75-A for inspection relief of external piping
(ECP < -230mV, HWC availability > 80%) F.O.I=1/6 (when ECP=- 300 mV,HWC avail.=100%)
 - Possible hydrogen demand change after power uprate(1.7% MU → 3% S)

國際接軌, 46 members BWR chemistry monitoring and assessment program

- ■美國核能界促進方案(Initiatives)下，35部US BWRs至今 HWC/NMCA/OLNC + DZO 無悔策略
(2008 德國柏林國際核電廠水化學會議)

核一、二廠未來 Possible IGSCC mitigation improvements

- ◆ HWC availability increasing (target 95%)
- ◆ Hydrogen injection during plant start-up ►
- ◆ NMCA/OLNC ►

大綱 II

OWC in Taipower PWRs



Primary side

- Improved Maanshan's RCS Li-B control program
- Zinc addition project at Maanshan has been suspended based on the calculation by WH VIPER/BOA code
- A campaign of shutdown chemistry control optimization since MS-2 EOC-16

Secondary side

- Maanshan's steam generator sludge pile management program

SG sludge source term reduction method

FW Fe control (Hydrazine , ETA Addition)



Consideration on adding Dispersant during SG wet layup in RFO

SG sludge removal method

Modified ASCA

國際接軌, 129 members PWR chemistry monitoring and assessment program??



大綱 III

Other Interesting Topics on EAC mitigation from Water Chemistry Perspective

- ◆ **Corrosion Fatigue of Stainless Steel in Low ECP BWR/PWR Environment** ☹
1998 Estimation of Fatigue Strain Life Curves for Austenitic SS in LWR Environments by ANL O. Chopra
1999 Robin Jones EPRI , cumulative fatigue usage factor(CUFs) may >1 in 60 Years
2001/2002 Fatigue Crack Initiation in Austenitic SS in LWR Coolant-A Review by ANL O. Chopra , Bill Shack

2002 /2004 /2006 Corrosion fatigue crack growth of 304 SS by SERCO UK David Tice

2007/2008/ 2009 Corrosion fatigue behavior (Initiation & Propagation) of Austenitic SS in LWR Environments by Switzerland PSI H.P. Seifert , S. Ritter

Water Chemistry Parameters (NWC vs. HWC) only have a little effect



- ◆ IASCC mitigated by HWC ➤

- ◆ PWR PWSWC Chemical Mitigation

Elevated DH₂ benefit on PWSWC growth rate

However , (Molander of Studsvik , Macdonald of Penn. State Univ., Japan) all indicate elevated DH₂ accelerates initiation of PWSWC

Decreased DH₂ Japan , JAPC

Zn Addition ➤

Li concentration (The effect of Li concentration on PWSWC growth rate show no or little influence. But,higher Li on initiation of PWSWC has not been investigated)

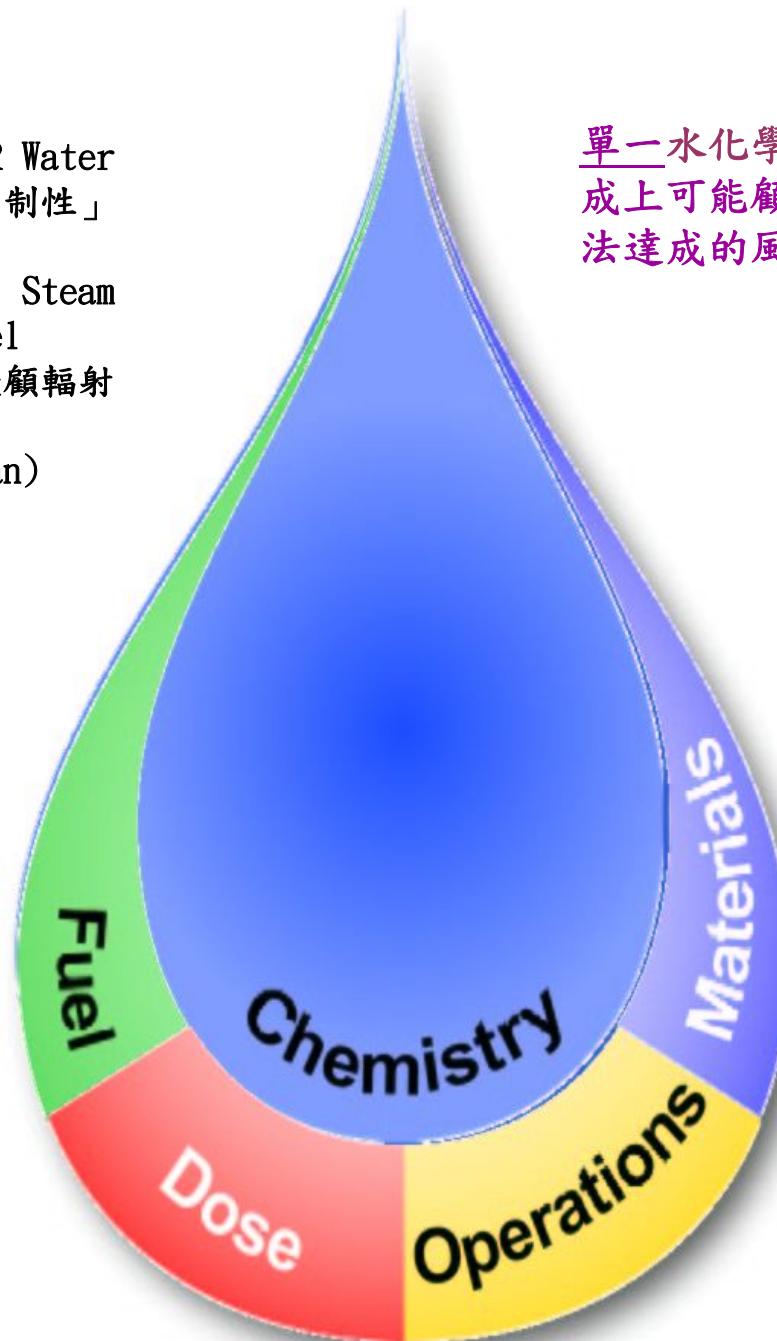
Some times the effects of these environmental parameters on PWSWC initiation and growth are different ----- by Molander of Studsvik NPC'08 Berlin

- ◆ SCC of stainless steel in stagnant lines attached to PWR RCS piping and components
Oxygen entrapped inside , high oxidizing environment ➤



臺電核一二三廠依據EPRI BWR/PWR Water Chemistry Guidelines 內唯一「強制性」要求，已建立以保護電廠資產(例如 Structure Material Integrity , Steam Generator Tube Integrity , Fuel Failure Free 等)為首要目標且兼顧輻射場劑量抑低之策略性水化學計畫
(Strategic Water Chemistry Plan)

單一水化學控制方式在各別目標達成上可能顧此失彼，增加各別目標無法達成的風險



美國的笨蛋(STUPID)諺諧文化

- 笨蛋，問題在經濟 199? 美國柯林頓競選總統
- 笨蛋，問題在經濟 2007 台灣馬英九競選總統
- 笨蛋應非罵人之髒話
而是振聾發聵、醍醐灌頂、點醒眾生之意



笨蛋，電廠水化學最適化控制關鍵是ECP & pH

日本JAPC前執行副總(顧問)Dr. Meguro解釋BWR/PWR機組如何分別以ECP(Electrochemical Corrosion Potential, 電化學腐蝕電位)及pH 酸鹼值之水化學方式來控制最影響 Structure Integrity與 Capacity Factor的材料劣化問題: IGSCC(應力腐蝕龜裂)+FAC (流體加速腐蝕/薄化)

---2007 亞洲核電廠水化學與腐蝕研討會

--- 2008 德國柏林國際核電廠水化學會議



從ECP及pH酸鹼值控制看臺電 BWR / PWR 水化學最適化控制策略的形成與進展

核一,二廠 (BWR)
ALARA (Purer Better) Chemistry (NWC)
水質控制 紀元



不鏽鋼/鎳基合金 IGSCC

Additive Chemistry (HWC/NMCA/OLNC)
(水質 + ECP ↓) 控制 紀元
↓ 碳鋼管路 FAC concern

FW 注氧(ECP ↑) / 管路薄化監測計畫

Impact on 乾井 Radiation Source Term
↓ Co-60 Deposit
DZO 加鋅水化學
↓ Fuel Crud/Corrosion concern
Under Limits of 2008 年 EPRI BWR Water Chemistry 指引

Impact on MSLR
HP Skyshine Management Program

ECP(Electrochemical Corrosion Potential, 電化學腐蝕電位) ↓ 愈低愈好 ???

ECP of 不鏽鋼/鎳基合金 ↓ IGSCC ↓ Co-60 Deposit ↑ (except 加鋅)

ECP of 碳鋼 ↓ FAC ↑

BWR Bulk Water pH 酸鹼值 ↑↓, Crevice pH 酸鹼值 ↑↓

PWR Bulk Water pH 酸鹼值 ↑, Crevice pH 酸鹼值 ↑↓

核三廠 (PWR)

一次側 Additive Chemistry (加氫, 氫氧化鋰, 硼酸)
鎳基合金 PWSCC / Primary Coolant Activity / AOA

(水質 + ECP ↓ + pH_T 微鹼) 控制最適化

+ DZA 加鋅水化學

二次側 Additive Chemistry (全揮發性處理, 加聯胺)
加乙醇胺ETA

鎳基合金 IGA/ODSCC, 碳鋼 FAC → Fouling of S/G

(水質 + ECP ↓↑ + Bulk pH 鹼性控制最適化
Crevice pH 趨中性)



HWC Effectiveness for IGSCC Mitigation

成效評估 (HWC決策前)

依據實驗室或In-Plant Bypass Loop Autoclave或In-reactor IGSCC initiation/growth
304 SS specimen 數據 (CERT / Fracture Mechanics CT / LPRM DCB)

Crack Growth Rate Reduction F.O.I. (HWC crack growth rate=NWC crack growth rate= 1/xx)

Toshiba 依據庫藏ECP vs. 304 S.S. crack growth rate 關係圖評估Chinshan and Kuosheng FW H2
0.5 ppm 時

CS RPV bottom 150 → 0.0 mV 1/11
KS RPV bottom 100 → -100 mV 1/25



工研院材化所 Kuosheng RWCU bypass loop ECP/CGMS FW H2 0.5 ppm 時 ECP=-120 mV, CT specimen
F.O.I. = 1/5

GE in-plant DCB specimen inside LPRM in upper core bypass region (close to top guide)
F.O.I. = 1/10

GE in-plant DCB specimen in BHDL F.O.I. = 1/22

成效追蹤 (HWC執行後)

◆ Spain GARONA NPP , Stub Tube (Furnace Sensitized 304 SS) HWC-M (1 ppm) , ECP -245 mV
UT inspection 深度 F.O.I. = 1/10

◆ 根據加氫前後 In-reactor core shroud UT Inspection 裂縫長度/深度量測 (by BWRVIP)

Six Plants - NWC

Two Plants - HWC

Two Plants - NMCA



F.O.I. = 1/2 ?



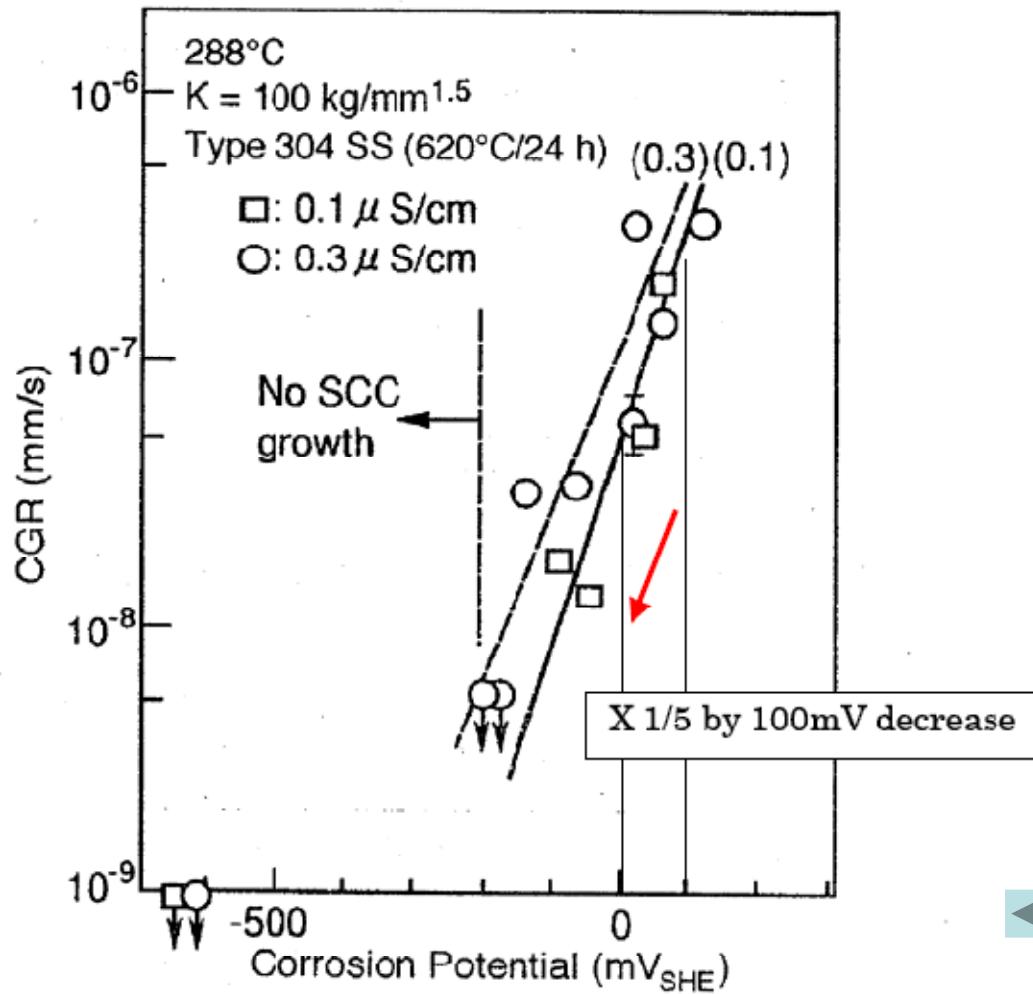


FIGURE 7. Effects of E_{corr} and conductivity on CGR of sensitized type 304 SS.

Fig.10 Correlation between crack growth rate and ECP of sensitized type 304 stainless steel
 (1) Kikuchi et al. (1997)

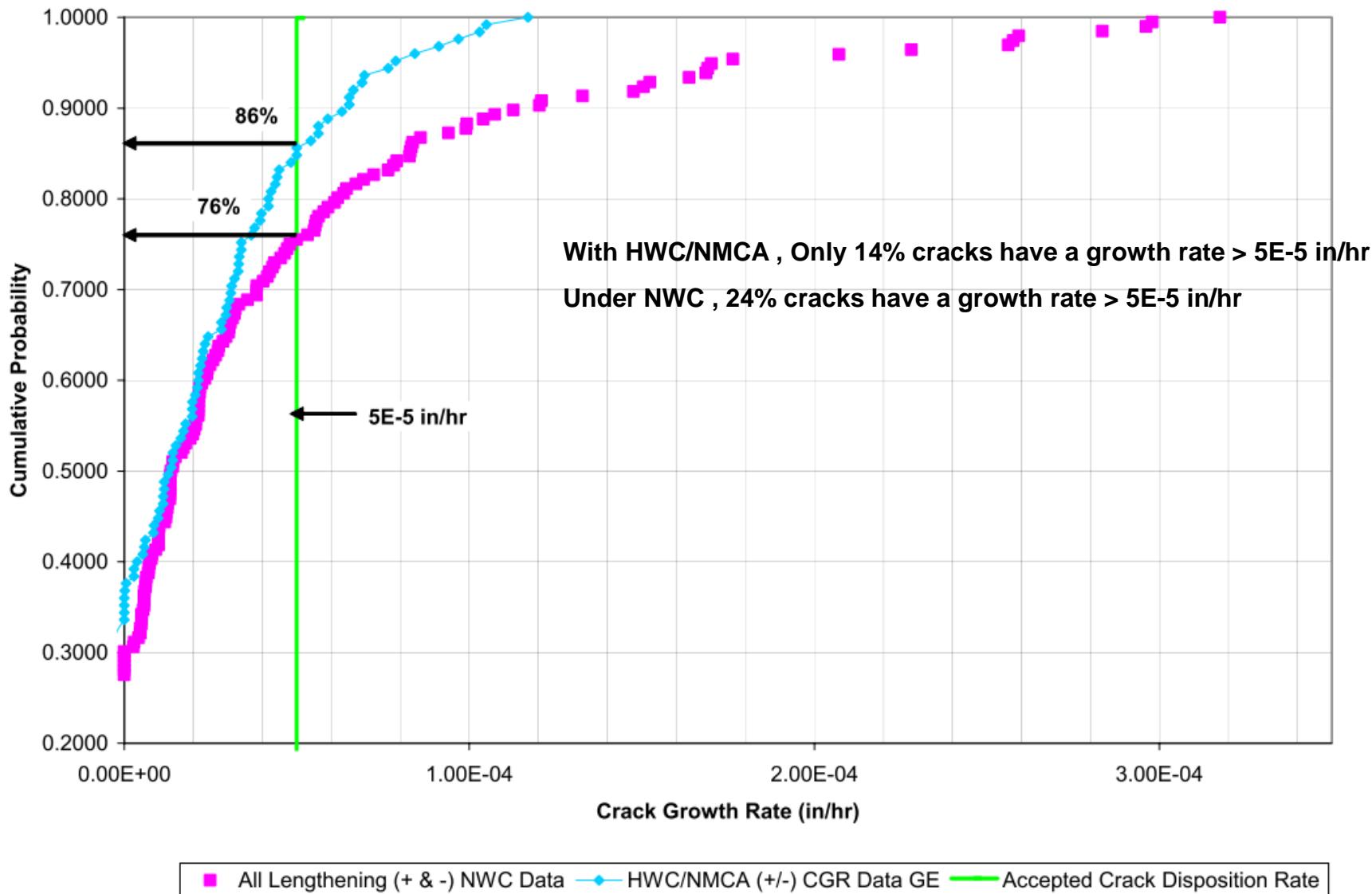


Figure 2-42
Lengthening CGR distribution NWC vs. HWC/NMCA for all plant [2-102]

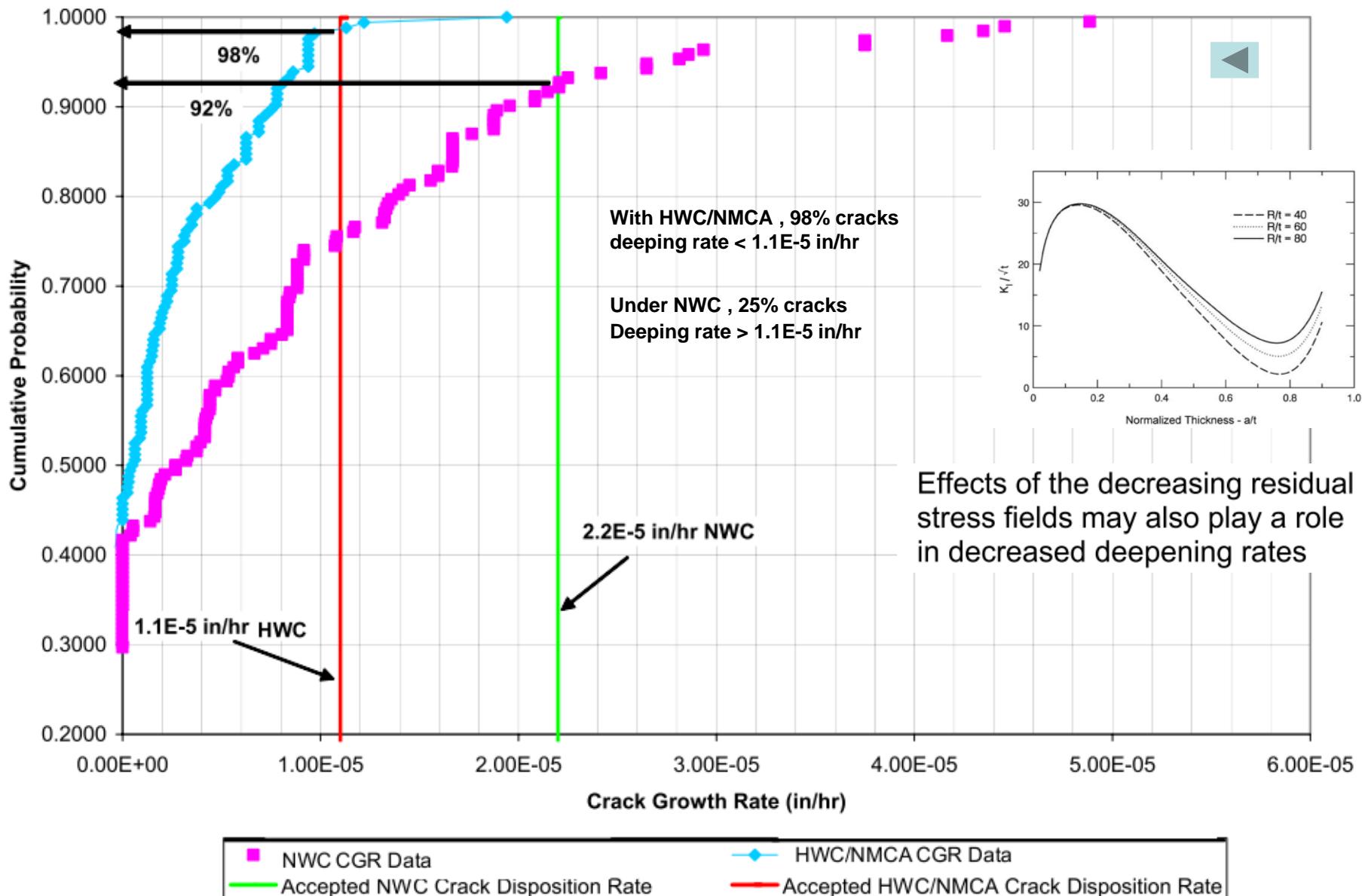
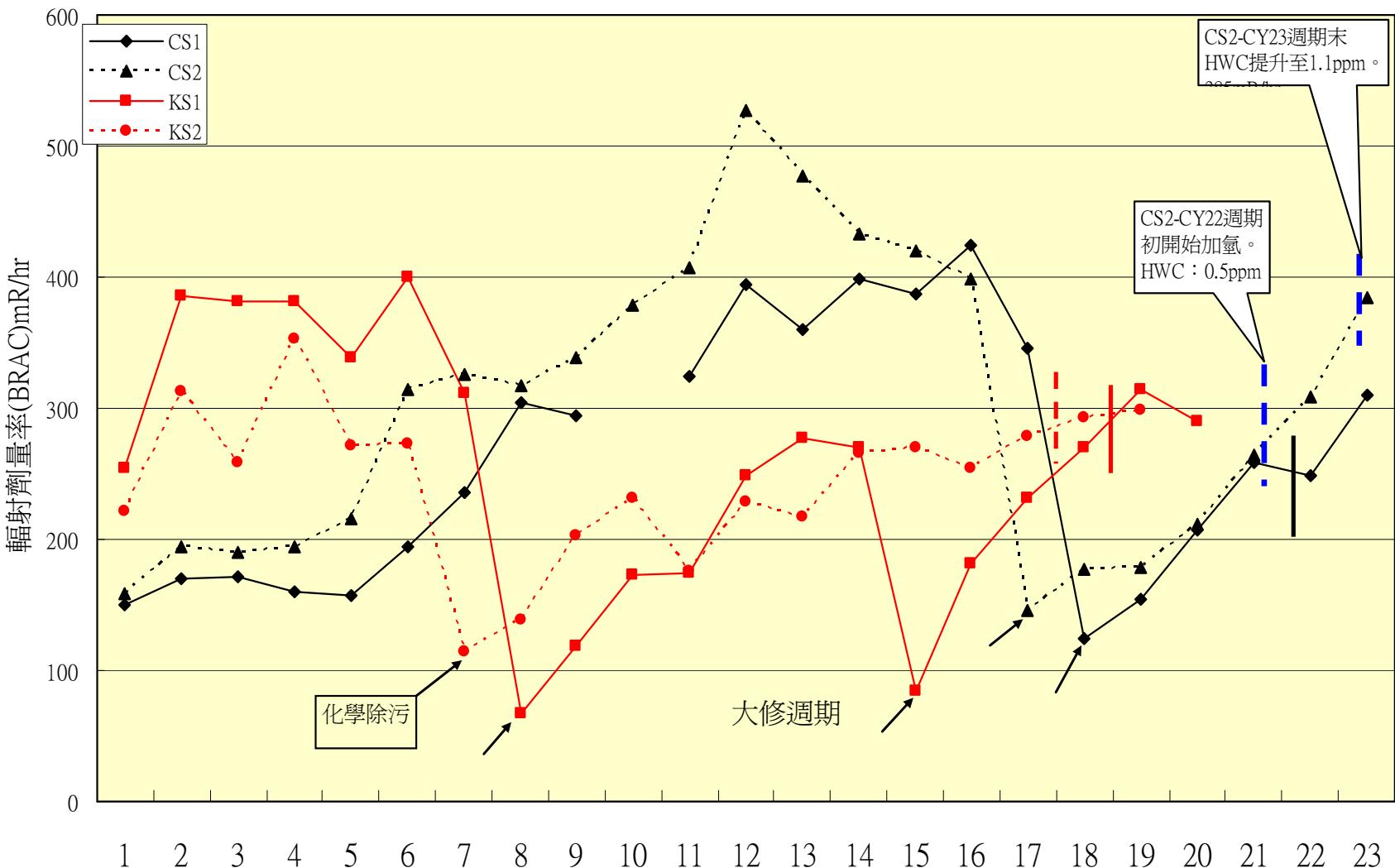


Figure 2-43
Depth CGR distribution NWC vs. HWC/NMCA for all plant [2-102]

核一、二廠四部機組再循環管路輻射劑量率(BRAC)趨勢圖



Shutdown Dose Rate Mitigation Strategies after HWC-M

- + (proactive 未雨綢繆 DZO + 系統化學除汙 + DZO) strategy-----核發處
Based on USBWRs/GE/EPRI post-HWC 經驗與建議

- + Reactive (臨渴掘井) strategy-----核一廠

a consideration on DZO will not be made until much higher dose rate increasing and intolerable after moderate hydrogen injection(> 1.0 ppm)

- + (乾井Shielding +系統化學除汙) strategy-----核二廠

1. DZO 對燃料護套 Crud/Corrosion 疑慮澄清

To Whom ? and On What ?

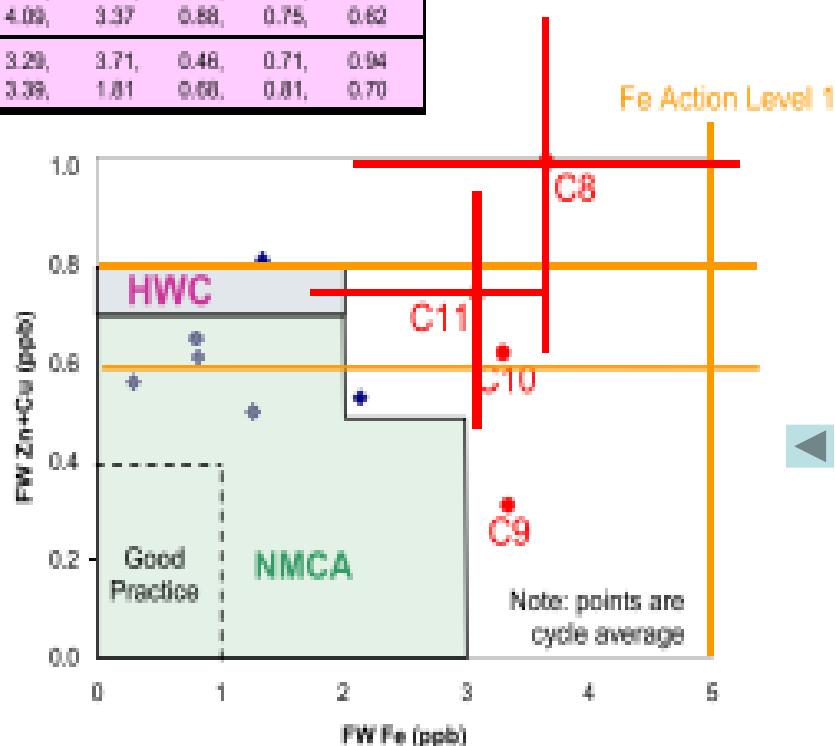


EPRI燃料部門 FRP and Limits on FW Fe, Cu, Zn

2. 核二廠燃料護套破損 without adding anything to RW. 加DZO後, 如發生Fuel Failure , 增加肇因分析複雜困難度.



	Cycle Avg. FW Fe (ppb)	Cycle Avg. FW Zn+Cu (ppb)	Quarterly Avg.			Quarterly Avg.		
			FW Fe (ppb)			FW Zn+Cu, ppb (Cu=0.2 ppb)		
River Bend C8	3.65	1.01	5.37, 3.17,	3.72, 4.09,	2.18, 3.37	1.33, 0.88,	1.28, 0.75,	0.94 0.62
River Bend C11	3.09	0.74	2.90, 3.45,	3.29, 3.39,	3.71, 1.61	0.48, 0.60,	0.71, 0.61,	0.94 0.70
Needed (Quarterly Ave)	2.0	<0.5						
Needed (Quarterly Ave)	3.0	<0.5						
FitzPatrick C17	2.14	0.53						
LaBalle-1 C11	1.35	0.81						
Grand Gulf C15	1.27	0.50						
PB-2 C18	0.30	0.56						
C08 C18	0.83	0.81						
VY C25	0.81	0.65						



Red bars in the figure are ranges of quarterly average Fe (horizontal) and Cu+Zn (vertical) for RB Cycles 8 & 11. Data points for RB Cycles 9 & 10 are cycle averages. Diamond points are cycle averages of other BWRs shown in the Table. Vertical orange line is FW Fe AL 1 of 5 ppb, and horizontal lines are limits of Cu+Zn for NMCA and Mod-HWC plants, respectively, in 2004 BWR Chemistry Guidelines

圖1:核一廠一號機CPD、CDE、FW不溶鐵變化趨勢

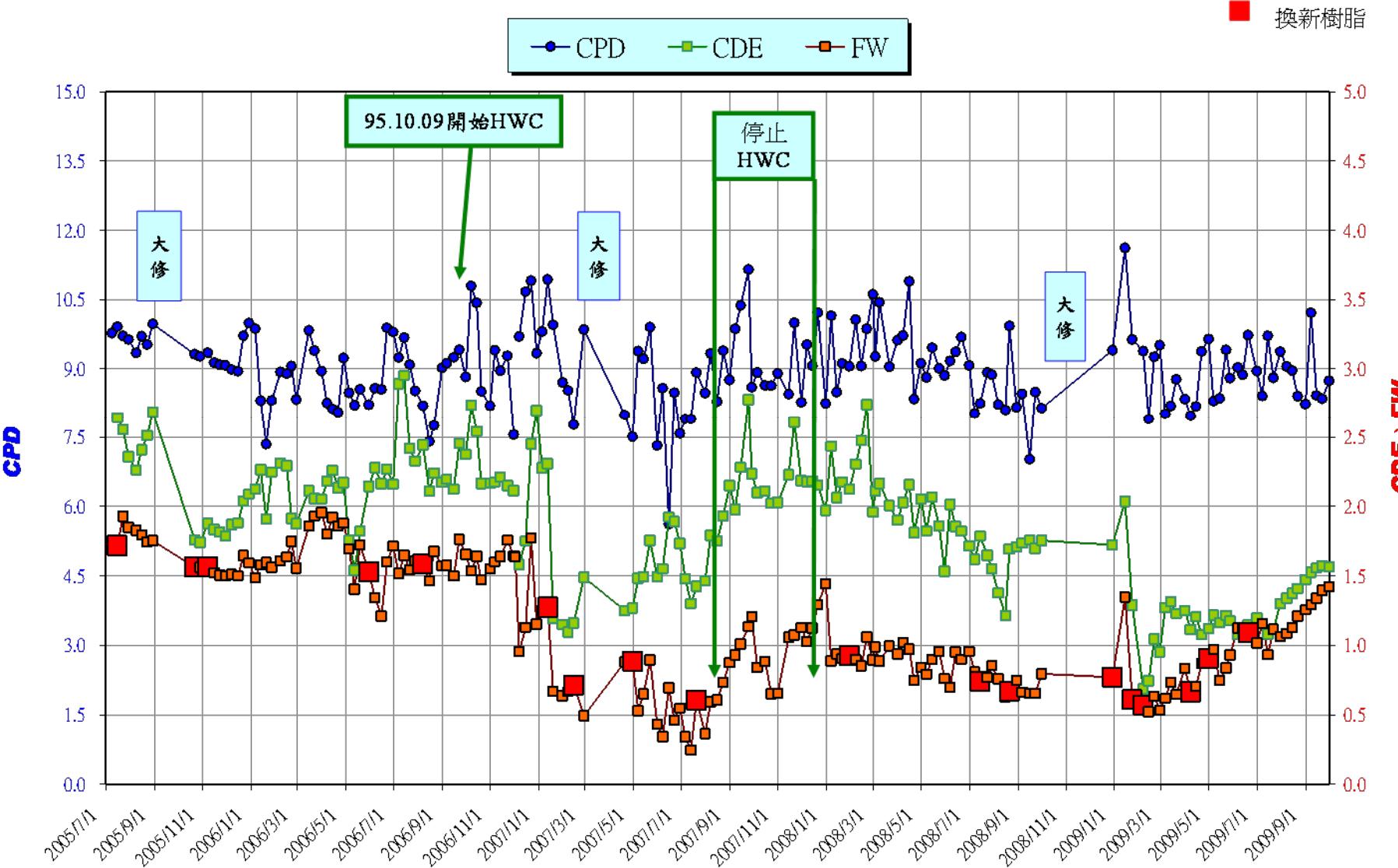


圖2:核一廠二號機CPD、CDE、FW不溶鐵變化趨勢

■ 換新樹脂

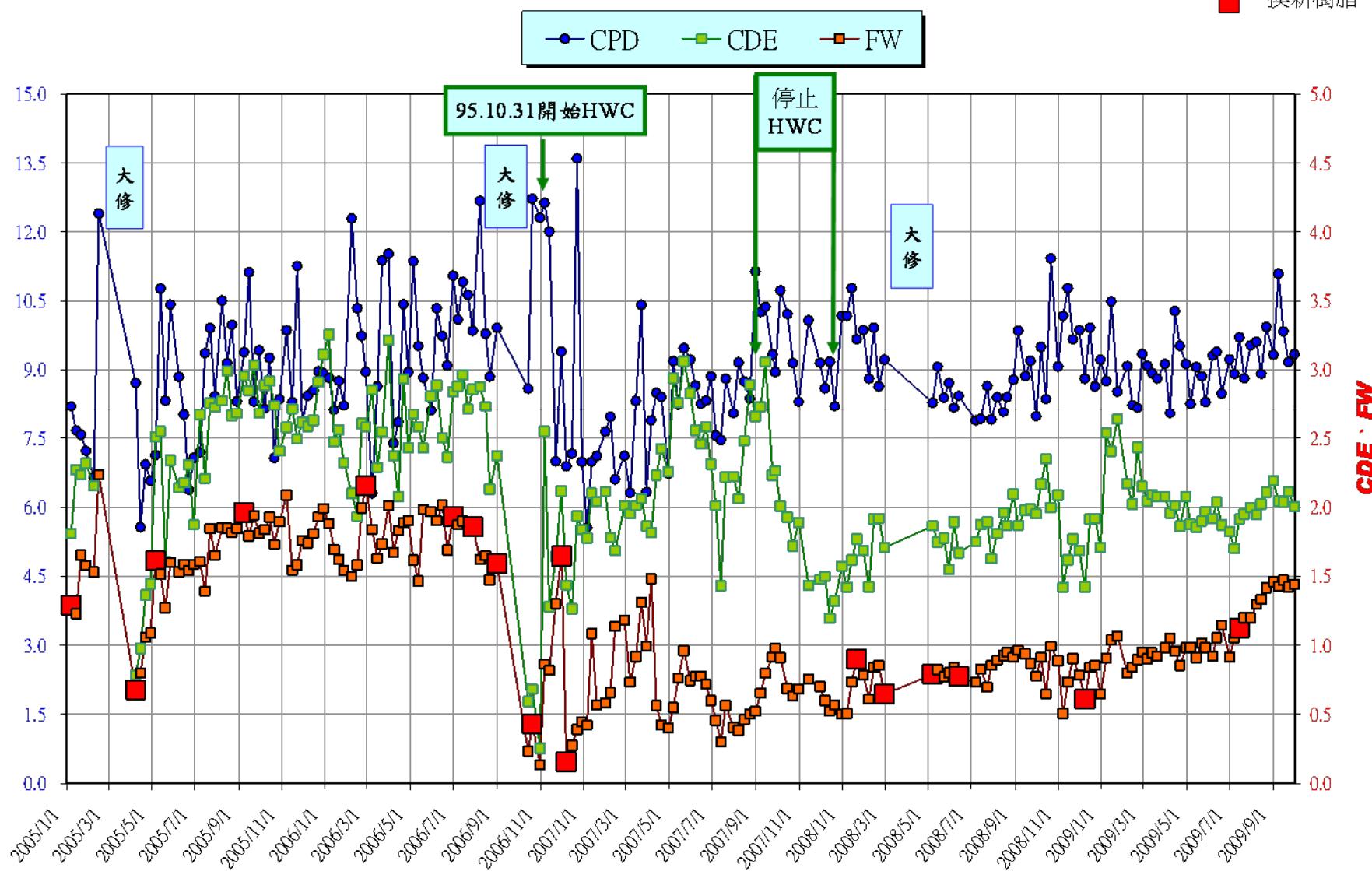


圖3:核二廠一號機CPD、CDE、FW不溶鐵變化趨勢

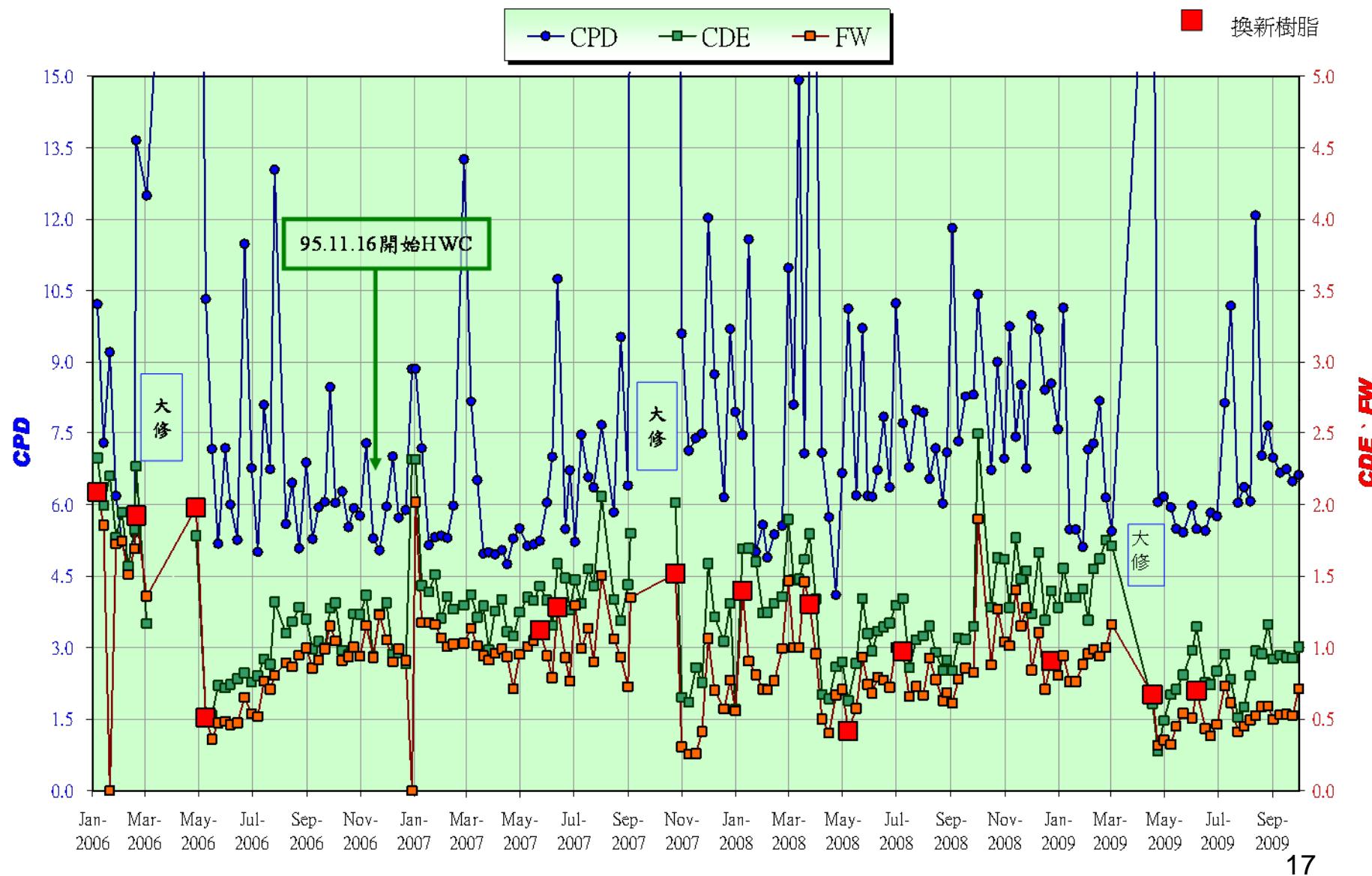
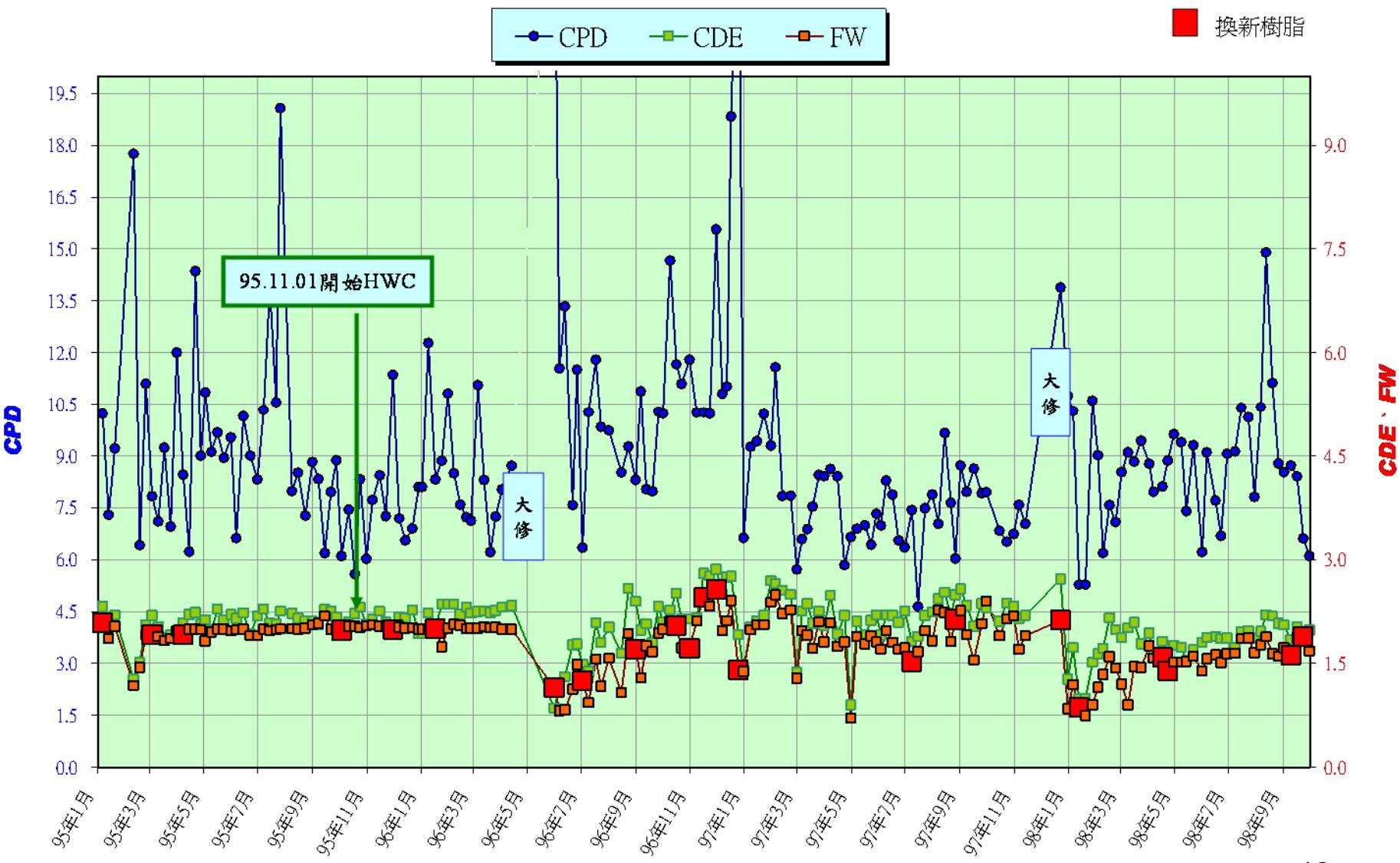


圖4:核二廠二號機CPD、CDE、FW不溶鐵變化趨勢



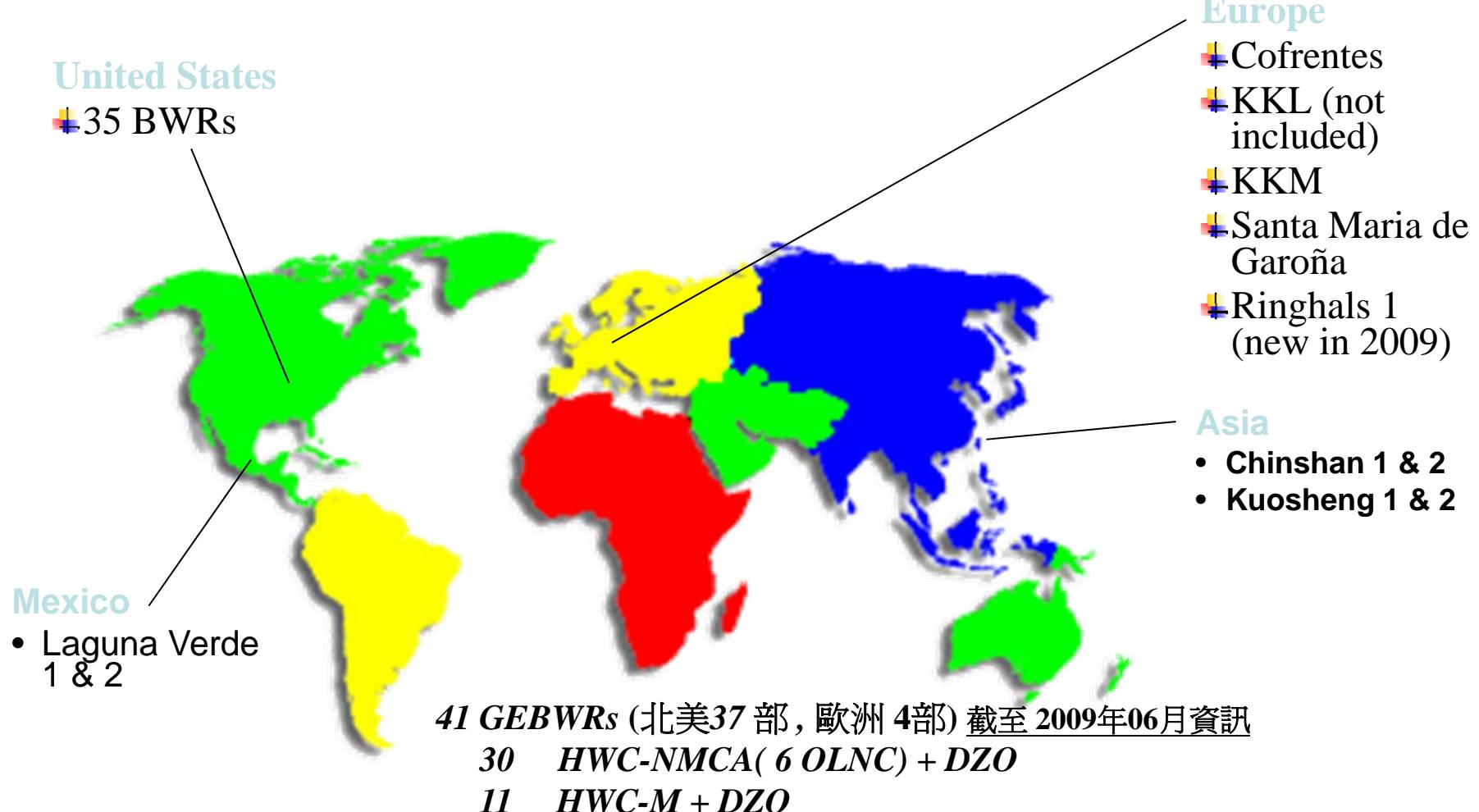



Kuosheng	Unit 1	Unit 2
Feedwater Iron (ppb)	0.92	1.9
Feedwater Zinc (ppb)	0.003	0.006
Feedwater Copper (ppb)	0.06	0.09
Reactor Water Conductivity (uS/cm)	0.079	0.082
Reactor Water Zinc (ppb)	0.92	0.85
Reactor Water Copper (ppb) before HWC	1.8	1.9
Reactor Water Copper (ppb) after HWC	1.2	0.8
Soluble Reactor Water Co-60 (uCi/ml)	8.7 E-5	7.1 E-5

It is believed that soluble copper is being reduced to a less soluble form in reducing regions of the reactor coolant system. Large increases in soluble RW copper are observed when the hydrogen injection system is taken out of service.



46 Participating BWRs



- 過去四年,US Nuclear Industry 開始 *major initiatives*(促進方案).
其中 3項衝擊到水化學.

1. Starting in 2004 , *Materials Degradation Initiative*

目標: controlling corrosion process

Key Part: EPRI Water Chemistry Guidelines

HWC 35/35 BWRs

HWC-M (ECP \leq -230 mV) 8 BWRs

NMCA/HWC (ECP \leq - 450 mV) 27 BWRs

OLNC/HWC 5 BWRs

希望經由ECP控制, 避免RPV Internals IGSCC 重大維修

2. Starting in 2005 , *Radiation Protection Initiative RP2020*

目標: to meet tighter regulatory limits in the future.

Key Part: Radiation Source Term Reduction

Water Chemistry is important in controlling the
the effects of source term

FW Fe 接近半數BWRs \leq 0.5 ppb

FW DZO injection 35/35 BWRs (except VY)

3. Starting in 2006 , *Fuel Integrity Improvement Initiative*

目標: Zero Fuel Failure by 2010

(包括考量水化學可能形成Fuel Crud and potential effects on fuel cladding corrosion)

高階主管認知後，水化學決策由上↓下

2008 EPRI BWR Water Chemistry Guidelines 建議

FW Fe 季平均值 < 3.0 ppb

< 2 ppb (when FW Zn > 0.5 ppb , Fw Cu < 0.05 pp)

< 2 ppb_(when Fw Cu > 0.05 ppb, FW Cu+Zn > 0.5 ppb)

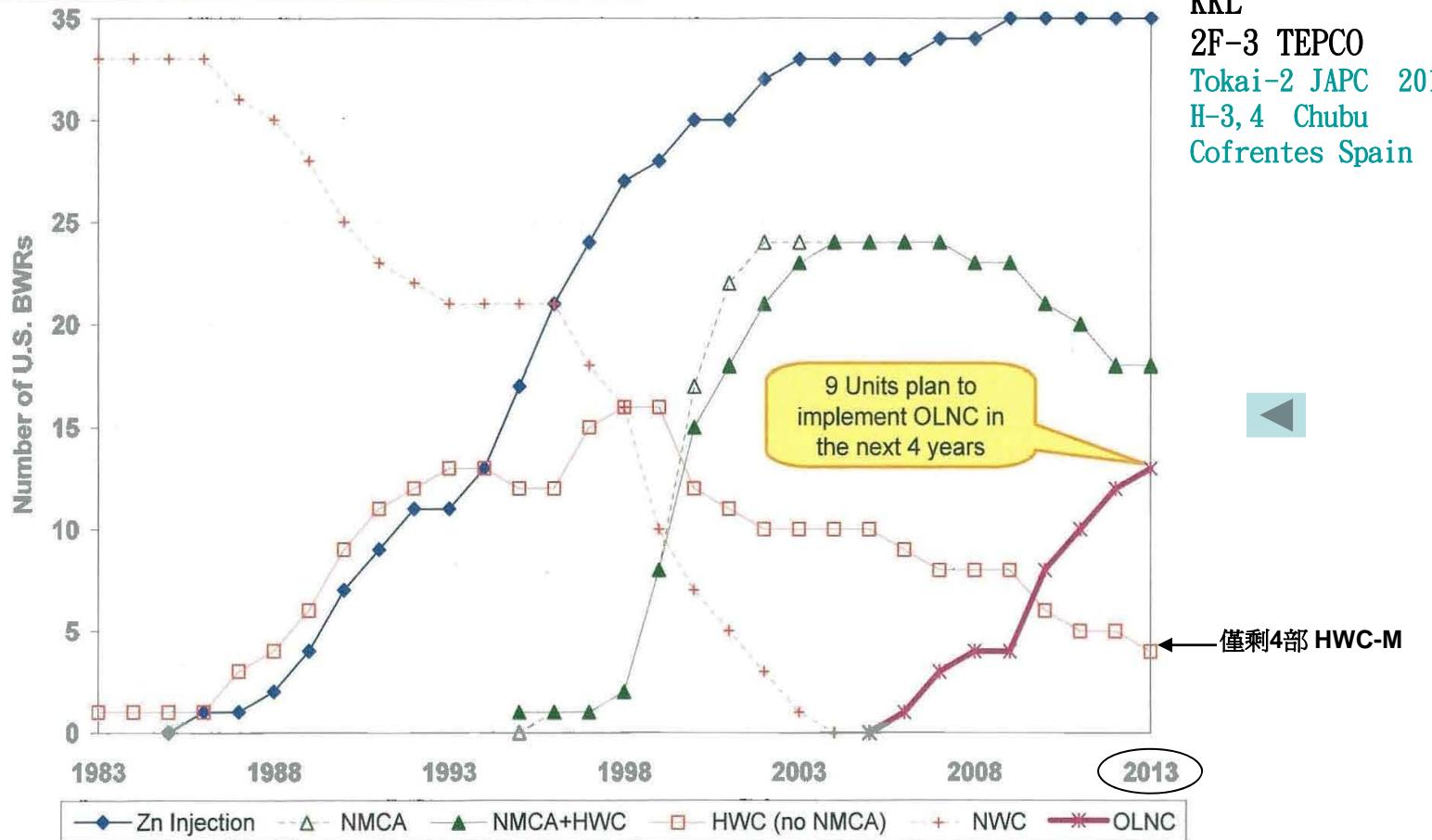
FW Zn 季平均值 < 0.6 ppb for HWC-M plants

FW Cu 季平均值 < 0.1 ppb

RW Si 季平均值 ≤ 300 ppb for Zn injection (good practice)

BWR Chemistry Trends in U.S.

Outside US
NMCA/OLNC
KKM
KKL
2F-3 TEPCO
Tokai-2 JAPC 2010
H-3, 4 Chubu
Cofrentes Spain



日本 HWC during Startup (HDS/DSHWC)

■ JAPC Tokai-2 (BWR-5) 與台電關係友好

HWC during Startup / RWCU H₂ injection one hour before plant startup
RWCU H₂ stop half hour after rated Rx water T/P
HDS 發表於 2005 亞洲核電廠水化學會議 (韓國主辦)
2007/ 9月 亞洲核電廠水化學會議(台電主辦)

■ Chugoku Shimane-2 (BWR-5) Kuosheng Sister

HDS Mini-tests in start-up of Cycle-15
will be automated in start-up of Cycle-17
發表於 2008 德國柏林國際核反應器水化學會議

美國 HWC during Startup (EHWC)

BWRVIP Chemical(Hydrazine)Injection to extend IGSCC mitigation from 93 C to 5% Power

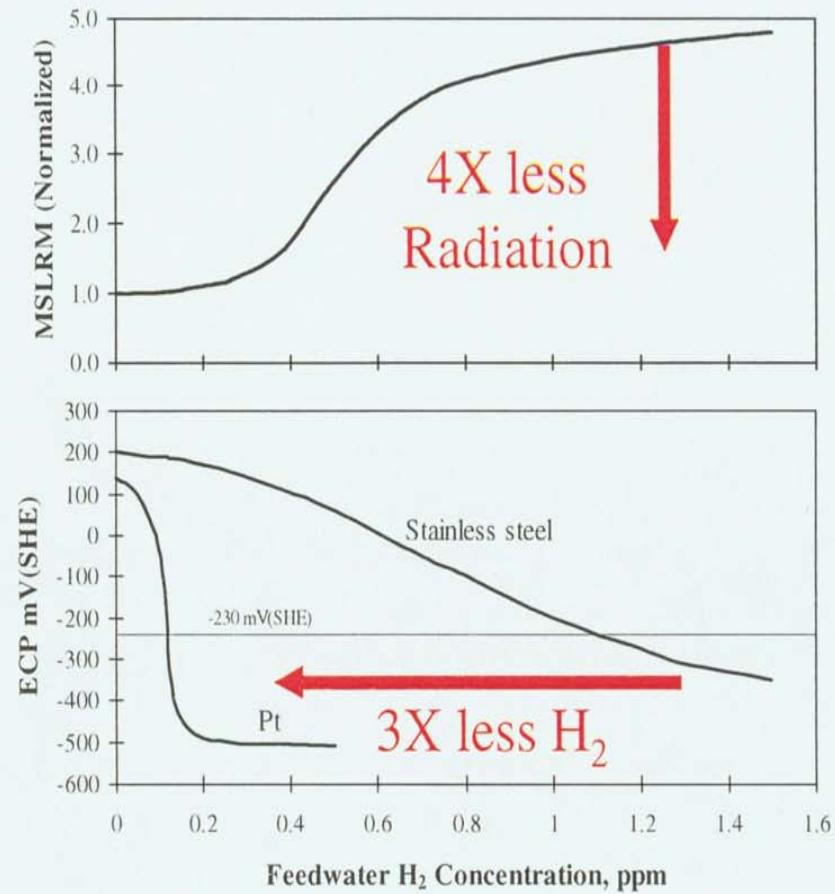
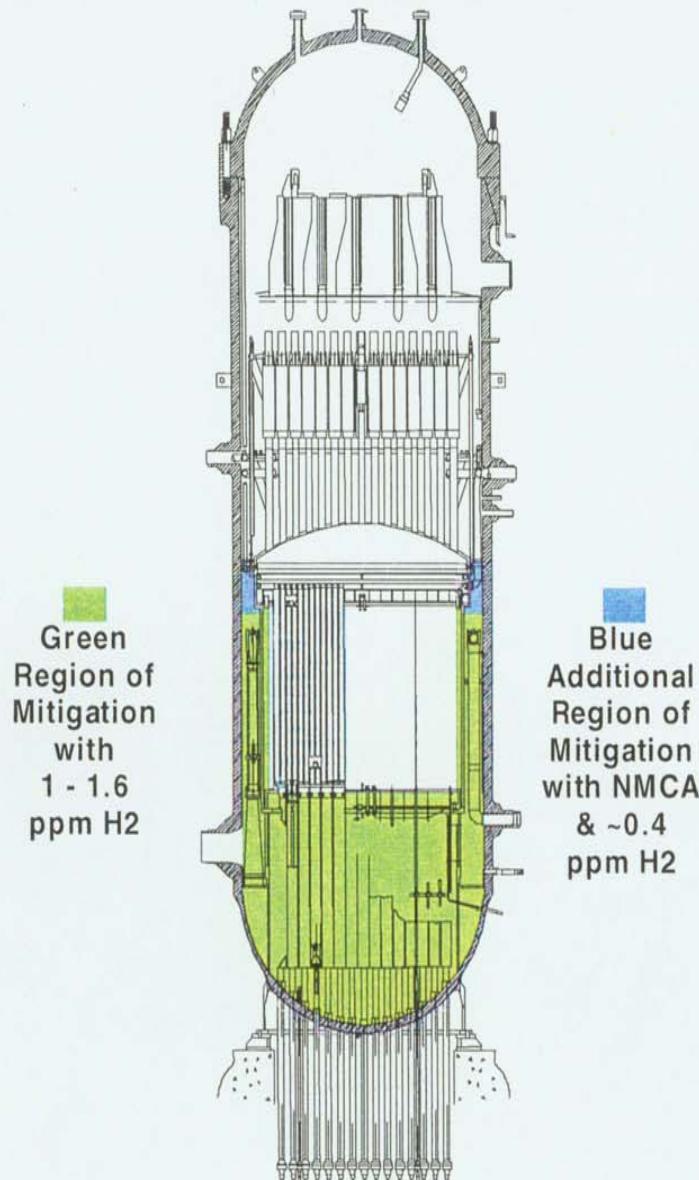
Hydrogen during Startup
(Early HWC)

Exelon PB-2 2010 demon.





NobleChem™ Benefits Over HWC



2013年前, US 4部HWC-M機組仍堅持不考慮NMCA/OLNC的理由

⊕ *Questions on its effectiveness: Knowledge GAP*

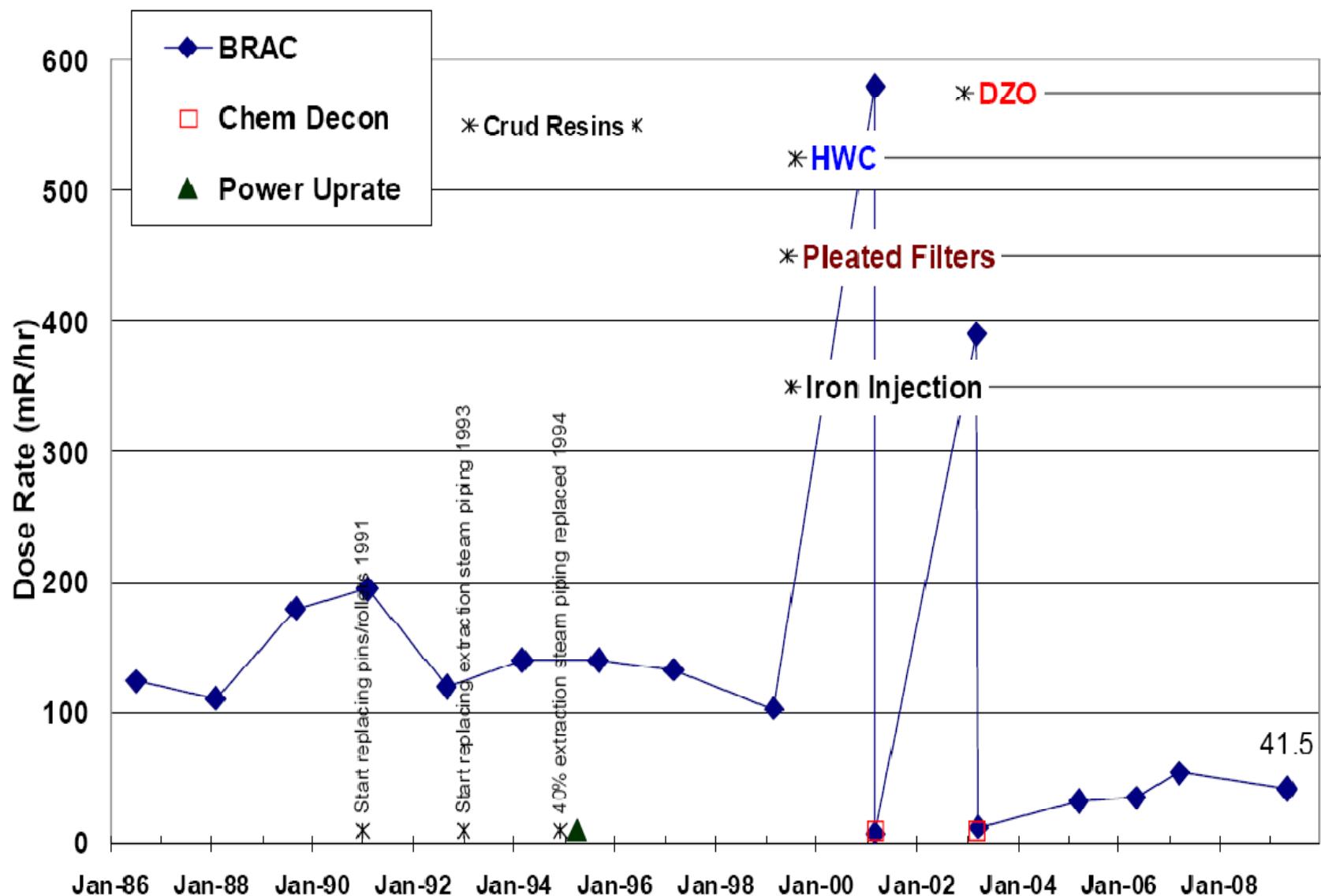
1. Although GEH has demonstrated that ECP is reduced following OLNC application , they have not demonstrated that it is being deposited in all areas where IGSCC mitigation is desired. There are also questions about whether enough noble metal deposits into low flow regions such as the annulus between the N2 nozzle and its thermal sleeve to provide IGSCC mitigation of nozzle and thermal sleeve welds. These welds are mitigated with Mod-HWC.
2. Crack flanking is not a concern with Mod-HWC. OLNC is intended to eliminate the crack flanking concern with Classic NMCA, but primary evidence that it does comes from KKM, where the shroud cracks are still growing, although at a slower rate

⊕ *Fuel Design groups are concerned :*

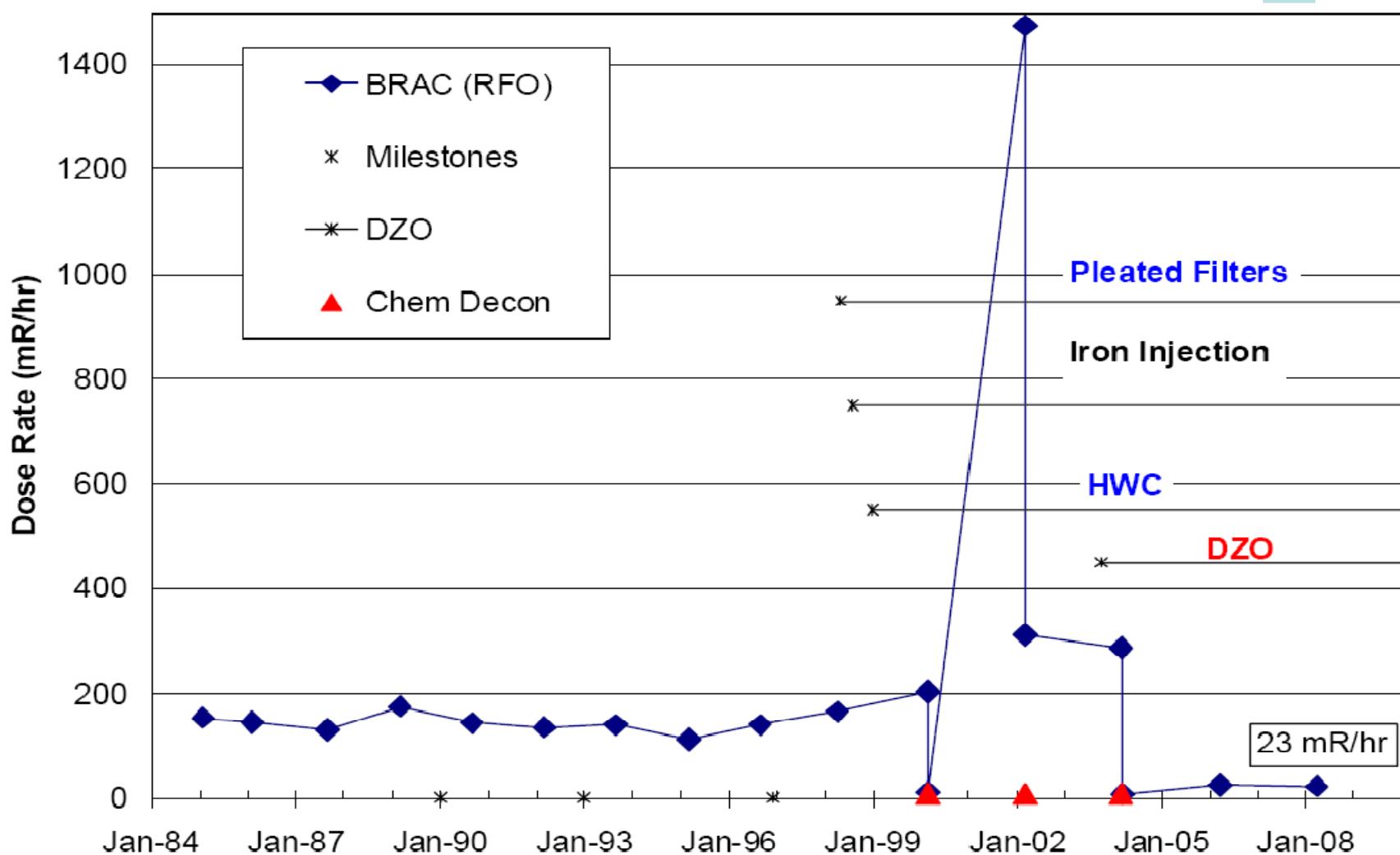
about the potential effects of noble metals on fuel corrosion (although none have been seen so far) and on hydrogen pickup by fuel channels, a factor in channel bow. Again, there is no theory and no evidence that suggests that either Mod-HWC or noble metal HWC causes or aggravates this situation, but the Susquehanna fuels people would rather not add noble metals

- 
- ⊕ Satisfied with shutdown radiation fields which have remained very low since the last round of chemical decontaminations, and satisfied with N-16 impact control.
 - ⊕ Two units has increased its capacity to inject hydrogen to ~110 scfm, sufficient to provide ~2.2 ppm FW H₂ following their Extended Power Uprate

Susquehanna 2



Susquehanna 1



- Core CIPS/AOA deviation more than -3% (MS-1 CY-16,17 and MS-2 CY-16)

RCS Li-B control was changed from modified pH chemistry to elevated constant pH (pHt 7.3) chemistry with Li concentration below 3.5 ppm since June 2006 (cycle-17 for both units)

- high radiation dose rate of SG channel head

Improved RCS Li-B control ►

RCS 5 ppb of Zn ☹

- WH type RCP No.1 seal abnormal leakoff events

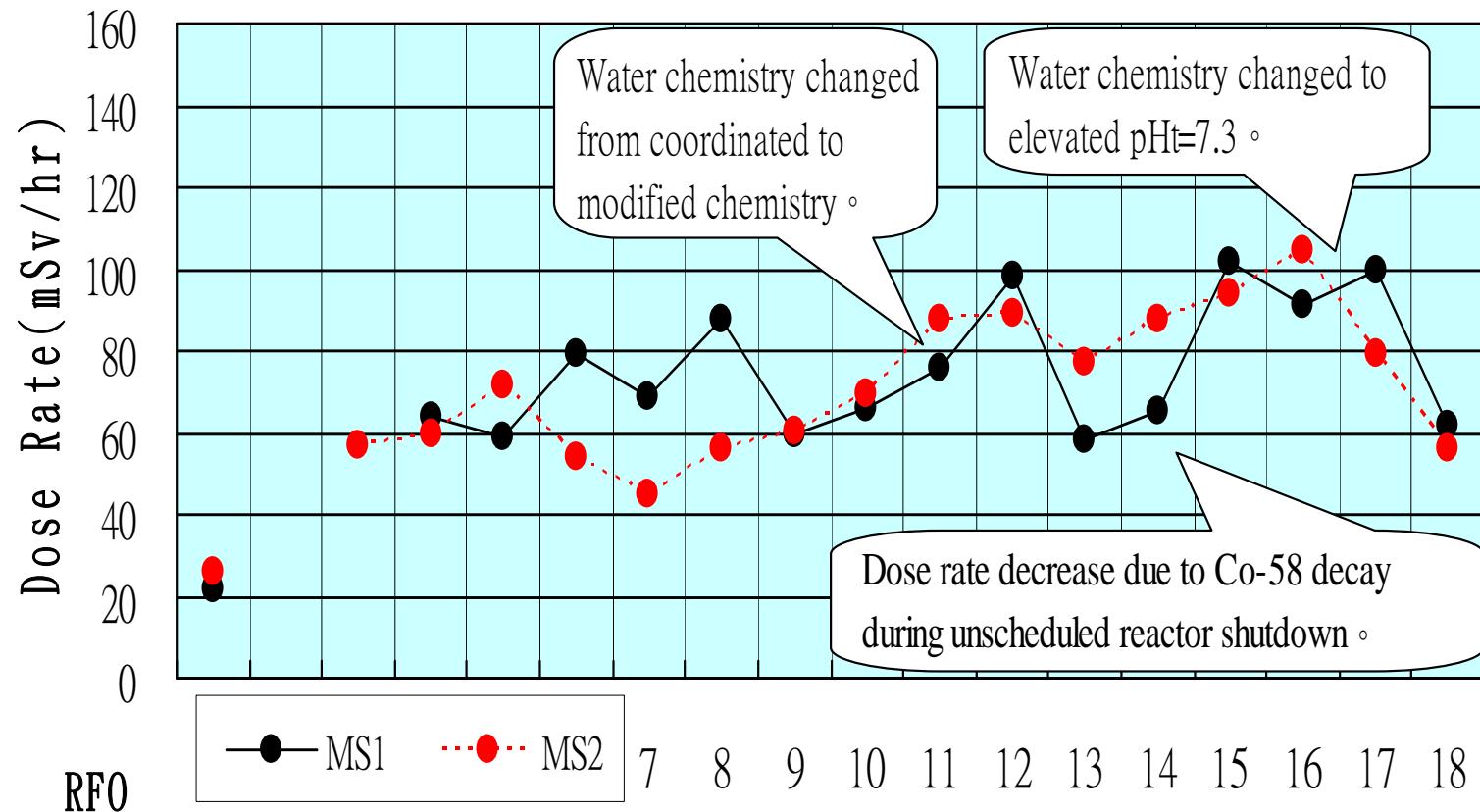
by a maneuver on *RCS chemistry in the end of cycle thru pH changes* (note:pH drop from 7.3 to 7.2) in addition to an increasing the amount and frequency of reactor make-up water , thereby disturbing the seal steady state conditions with a flushing action caused by cooler and oxygenated water. ►

- 大修人員劑量

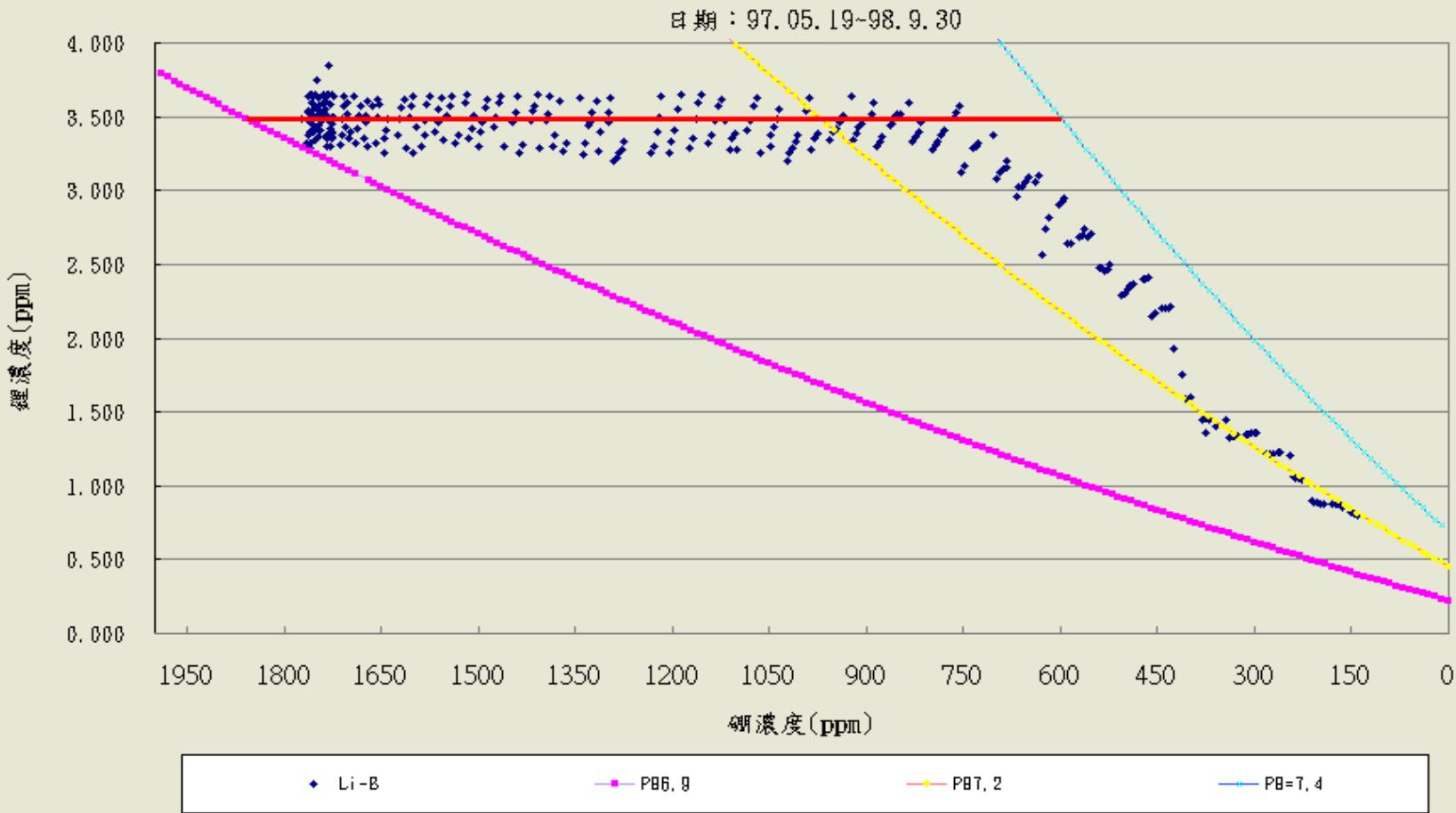
Through a campaign of shutdown chemistry control optimization since MS-2 EOC-16 , personal exposure for the work of RPV head open has been decreased from 73.67 man-mSv to 22.63 man- mSv exposed in MS-1 EOC-18



Maanshan#1#2 S/G Channel head Dose Rate Trend



二號機(Cycle-18)反應器冷卻水系統鋰、硼控制圖

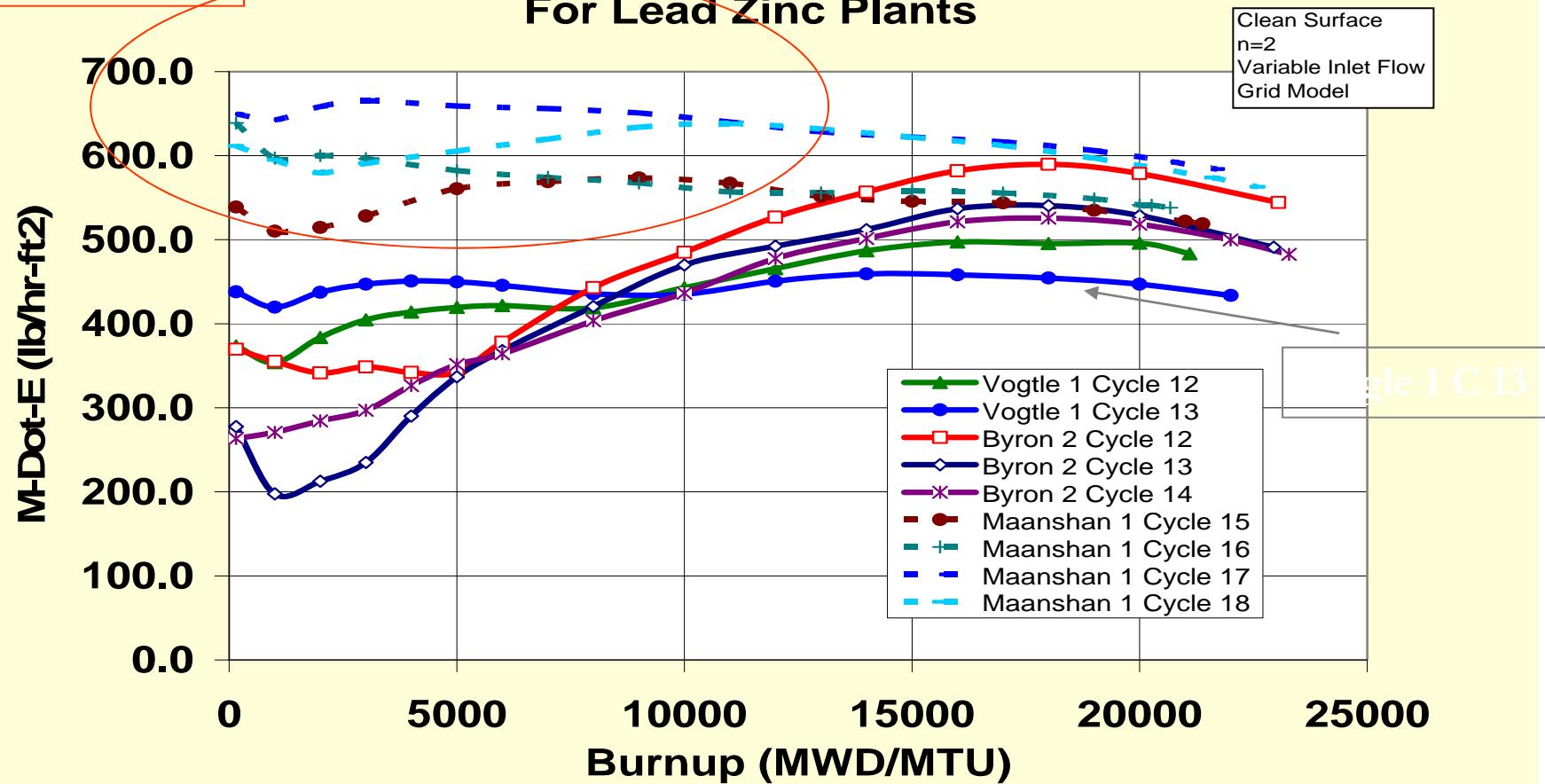


Maanshan 二號機CY-18 RCS酸鹼值長期維持於Tref300°C的 pH_T7.3已至燃料末期。
酸鹼值的控制非常小心謹慎

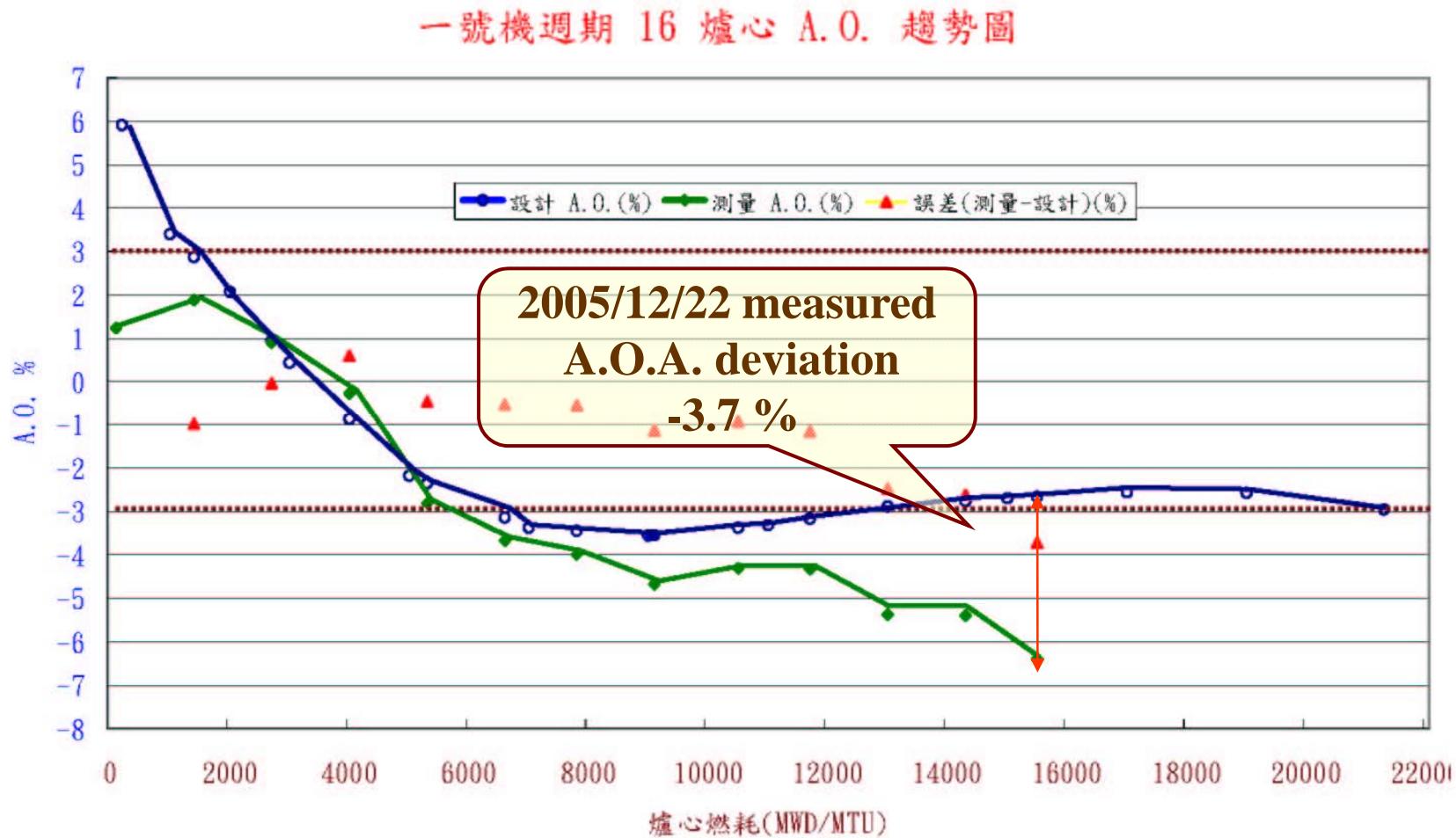


MS : High Sub-Cool Boiling Duty
 High Duty Core Index = 260
 High Coolant Temperature Thot = 621.5°F

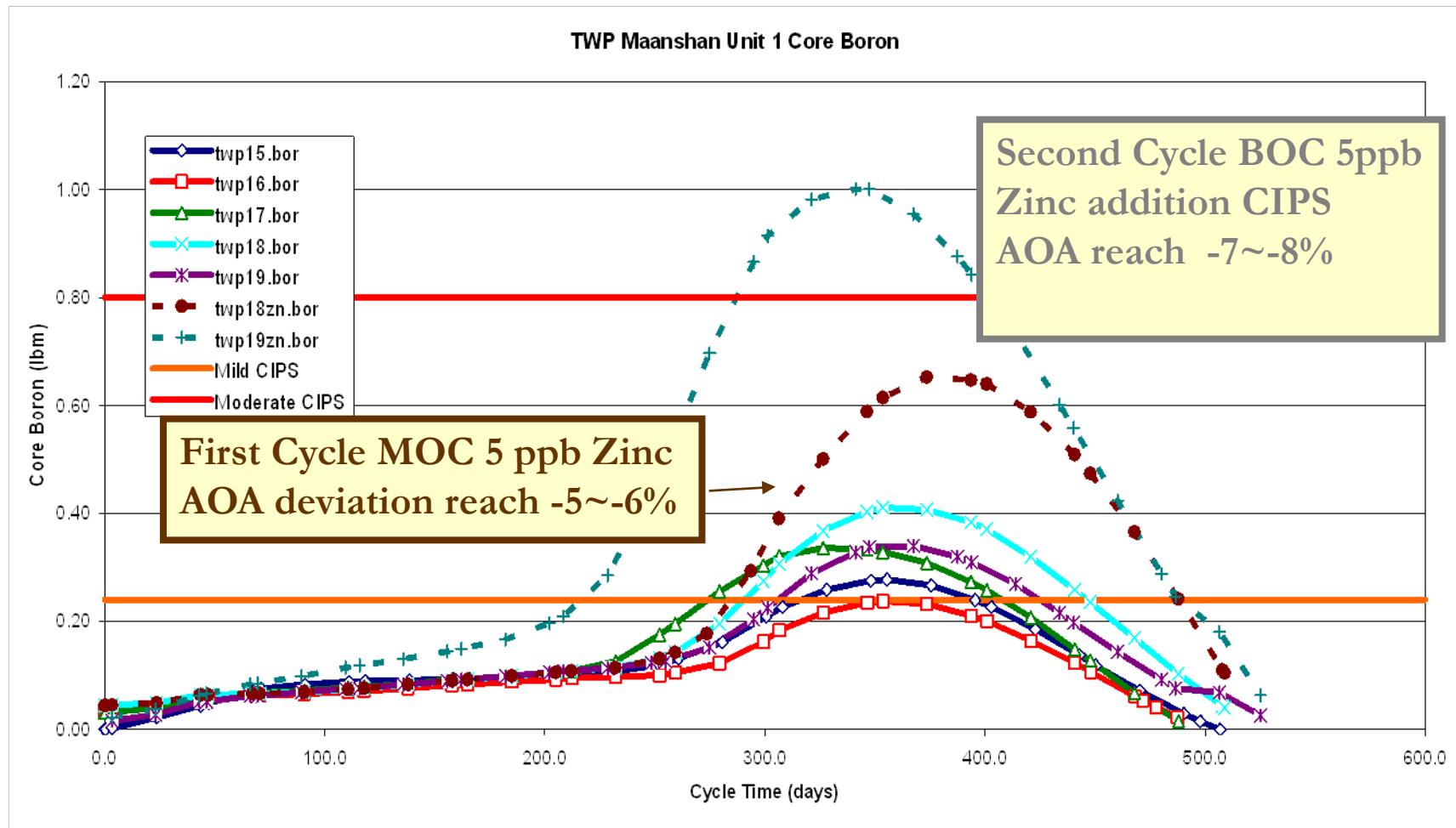
MS Boiling Duty **VIPER-W Maximum Local Mass Evaporation Rate For Lead Zinc Plants**



MS is now operating in CY18
MS CY16、CY17 got CIPS AOA problem



MS can't survive at even 5 ppb Zinc Addition Calculated by WH VIPER/BOA Code



TPC has suspended the MS DZO project



- ❖ TPC has suspended the DZO project account of following considerations:
 - ① Inherent Constraints of NSSS HD condition.
 - ② High surveillance cost for Zinc addition, including Fuel inspection, Fuel clean and Core design CIPS-Risk assessment.
 - ③ Need much more fuel cost for reducing the $F\Delta H$ in core design(4~8 million/cycle)



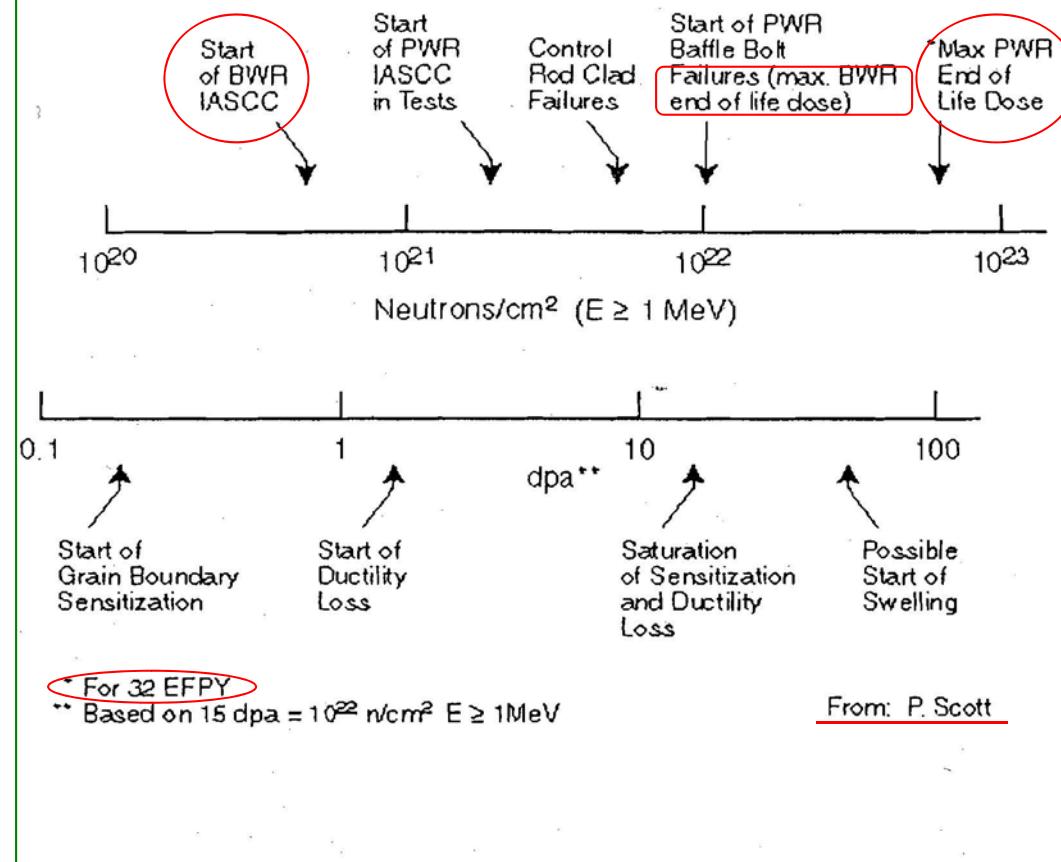
Comparison of Field Observations to Changes in Microstructure

HWC 抑低 core shroud 不鏽鋼 (exposed to $< 5 \times 10^{20} \text{ n/cm}^2$ neutron irradiation) IGS SCC growth rate 的效果雖已報告於 BWRVIP-14, 對接受更高中子通量下 (例如機組延役至 60 年) 之不鏽鋼是否仍能享受 HWC 的 benefit ? 後續 BWRVIP-99 研究指出 $5 \times 10^{20} \text{ n/cm}^2$ to $3 \times 10^{21} \text{ n/cm}^2$ 高中子通量下 HWC 仍具 benefit 。

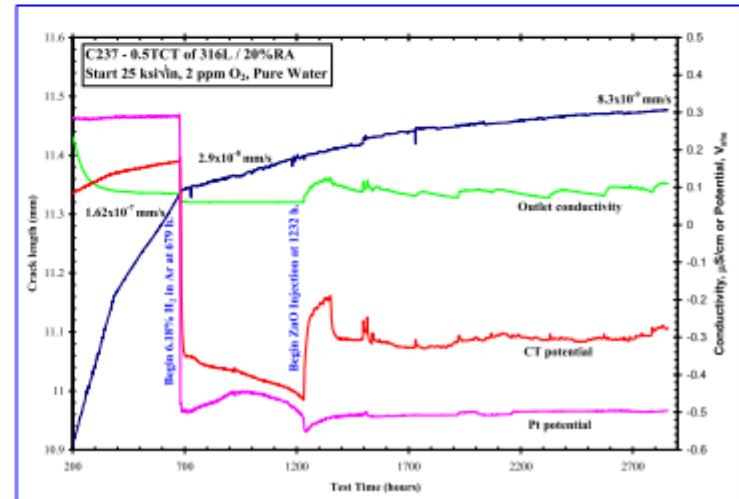
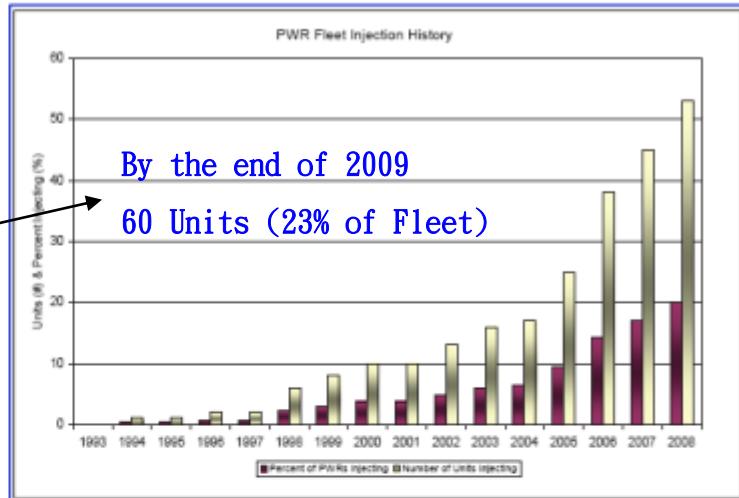
Followup to BWRVIP-99, phase 1 結果顯示 up to 6.7 dpa ($1 \text{ dpa} = 7 \times 10^{20} \text{ n/cm}^2$) HWC 仍能降低不鏽鋼 ECP, 但高於此中子通量後, HWC 似乎無效 。

HWC mitigates IASCC in SS at moderate K_s ($\sim 15 \text{ ksi/in}$) but may be less effective at higher stress intensities ($\sim 18 \text{ ksi/in}$) .

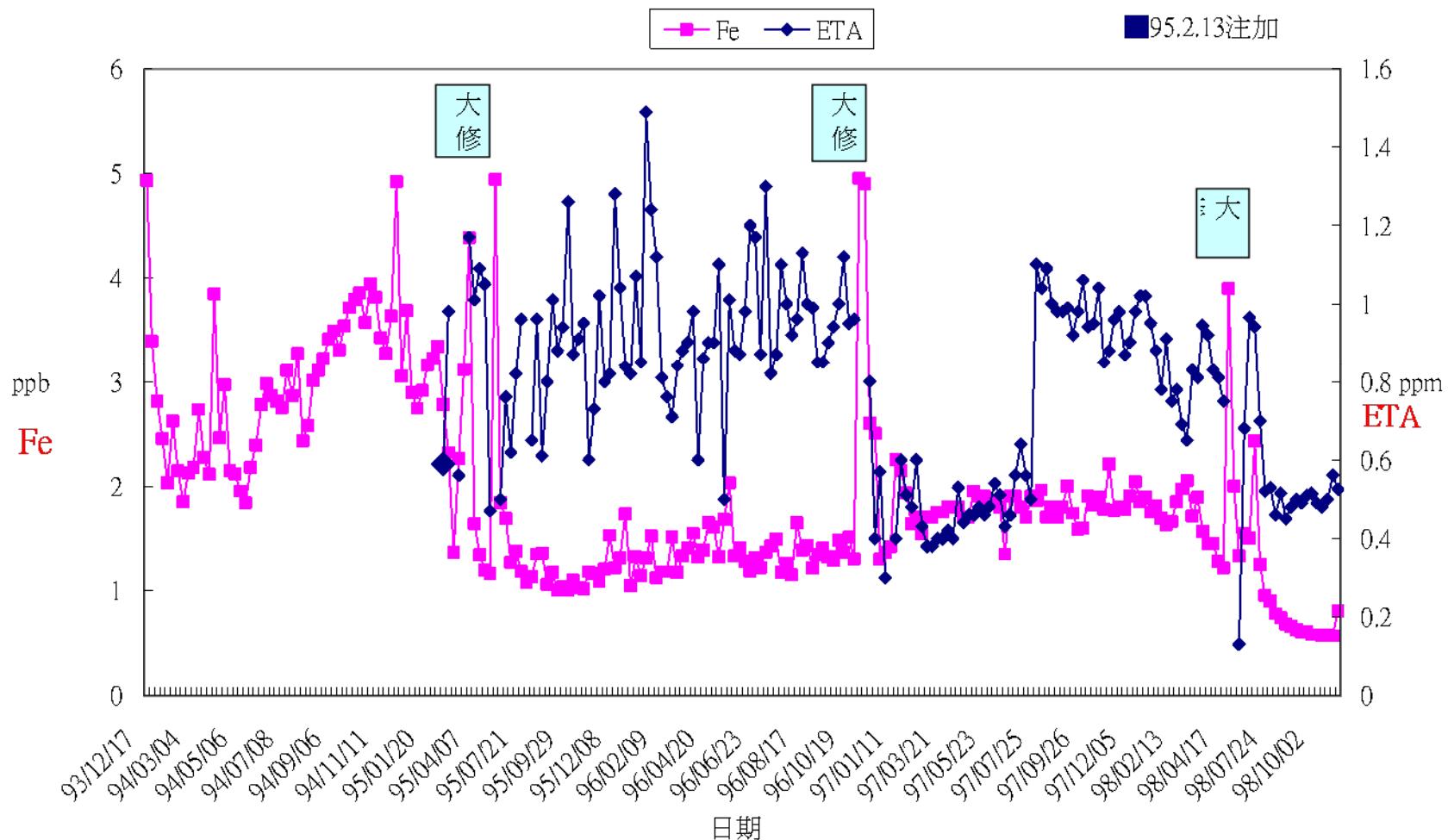
HWC is effective for non-irradiated stainless steels even at high K values



- Soluble Zinc Added for Exposure Reduction
 - Zinc addition in BWRs since 1986
 - Zinc addition in PWRs initiated in 1994
 - 50+ PWR plants worldwide now inject zinc
 - Fuel effect concerns currently limit maximum concentration
- Field and Laboratory Data Suggest Zinc Addition May Mitigate PWSCC
 - Clear effect for stainless steel
 - Steam generator tube inspection data show clear benefit for slowing time to initiation in Alloy 600
 - Picture less clear for mitigation of crack growth rate in Alloy 600 and 82/182 weld metals

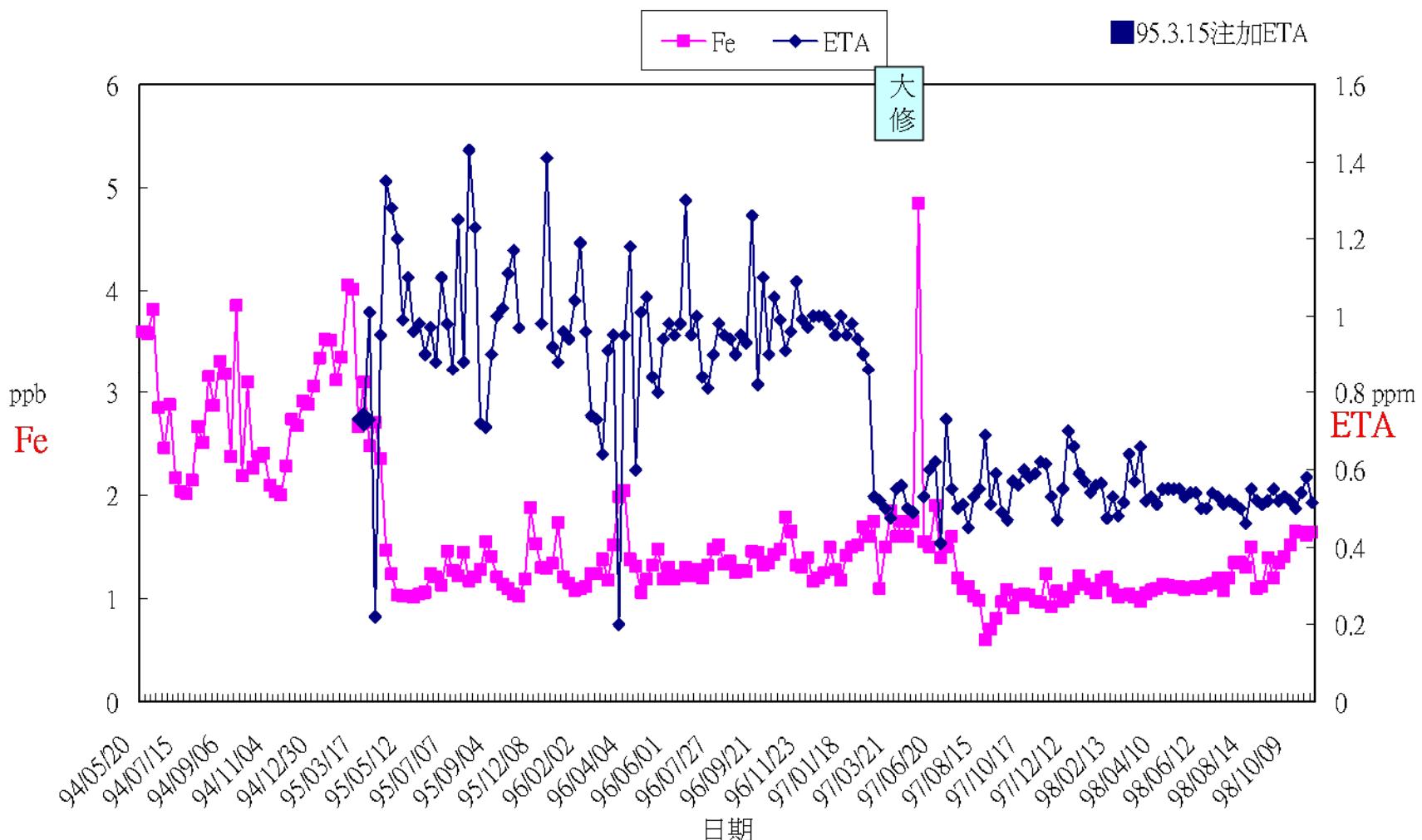


核三廠一號機飼水鐵及乙醇胺趨勢圖





核三廠二號機飼水鐵及乙醇胺趨勢圖



END

謝謝

敬請指教